E 1 = 28 SL_A - - 79 106

Aleph 12 11=20

SOLAR/2003-79/06

Monthly Performance Report





National Solar Heating and Cooling Demonstration Program

National Solar Data Program

NOTICE _____

This report was prepared as an account of work sponsored by the United States Government. Neither the United States nor the United States Department of Energy, nor any of their employees, nor any of their contractors, subcontractors, or their employees, make any warranty, express or implied, or assume any legal liability or responsibility for the accuracy, completeness or usefulness of any information, apparatus, product or process disclosed, or represents that its use would not infringe privately owned rights.

MONTHLY PERFORMANCE REPORT SCATTERGOOD SCHOOL JUNE 1979

SYSTEM DESCRIPTION

A solar energy system is installed at Scattergood School near Westbranch, which is located 35 miles southeast of Cedar Rapids, Iowa. The system is designed to supply approximately 75 percent of the annual space heating requirements for the gymnasium, as well as 75 percent of the hot water for the student locker room. This solar energy system is also used to dry grain in a modified grain silo located on the site adjacent to the gymnasium. The site has an array of 128 flat-plate collectors, manufactured by Solaron, with a gross area of 2,496 square feet. The collectors face south at an angle of 50 degrees from the horizontal. Collected solar energy is stored in a pebble bed containing 64 tons of stones for space heating and in two 120-gallon tanks to permit DHW preheating. Air is the medium used for transferring energy from the collector array to the pebble bed or directly to the gymnasium.

When solar energy is insufficient for space heating, two 250K Btu propane gas heaters furnish auxiliary energy. Auxiliary heating for hot water is provided by a 52-gallon domestic water heater containing standard electric resistance, immersion heater elements. The solar energy system is manually converted to summer mode operation by opening and closing slide gate dampers which isolate the storage from the solar energy system. The control system switch then is positioned to the summer mode.

The system, shown schematically in Figure 1, has five modes of solar operation.

Mode 1 - Collector-to-Space Heating: This winter mode is entered when two conditions occur simultaneously. The first condition occurs when the collector outlet temperature exceeds the gymnasium temperature by at least 45°F. The second condition occurs when there is a space heating

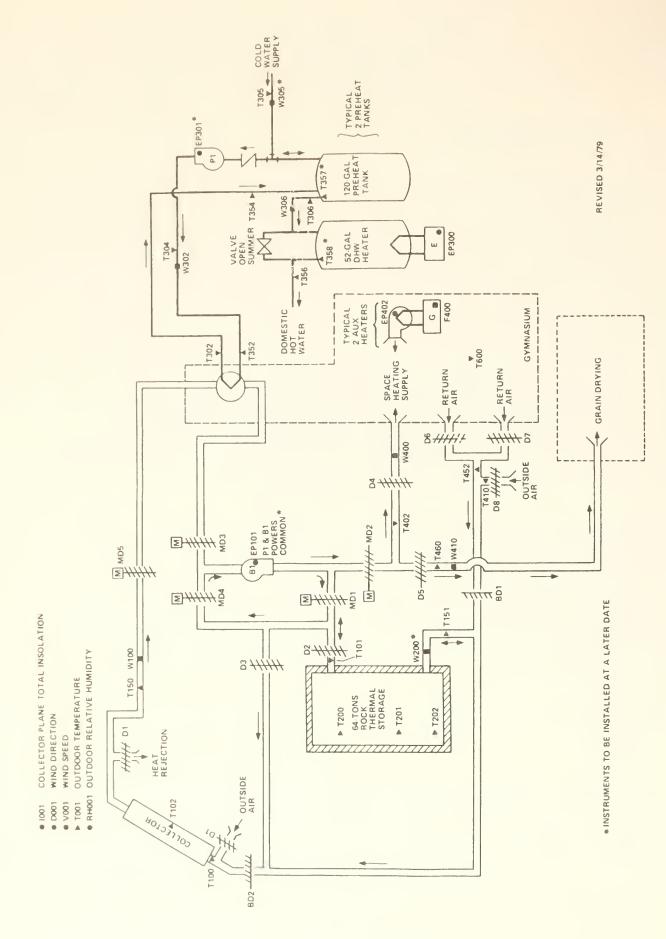


Figure 1. SCATTERGOOD SCHOOL SOLAR ENERGY SYSTEM SCHEMATIC

demand indicated by the manually preset, two-stage thermostat. The air heated by the collector is circulated by the air-handling unit between the collector and the gymnasium through ducts containing motorized dampers. In this mode, the heated air bypasses the rock thermal storage as it returns to the collector. This mode continues until either the collector outlet temperature no longer exceeds the collector inlet temperature by at least 30°F, or the demand for space heating is satisfied. Stage one of the thermostat operates when solar energy is needed, and stage two operates in conjunction with stage one to activate the auxiliary heaters to supplement solar energy when the gymnasium temperature drops below a level determined by the thermostat setting.

Mode 2 - Storage-to-Space Heating: This winter mode is entered when these three conditions occur simultaneously: 1) there is a demand for space heating, 2) the collector loop is not active, and 3) the temperature in the rock thermal storage is 90°F or higher. Air is drawn through the ducts from storage and circulated through the air-handling unit to the conditioned space and returned to storage; the air bypasses the collector.

Mode 3 - Collector-to-Storage: This winter mode is entered when the collector outlet temperature exceeds the gymnasium temperature by at least 45°F, and Mode 1 is not required. Heated air is drawn from the collectors, via the air-handling unit, and is circulated between rock thermal storage and the collectors. This mode continues until the collector outlet temperature no longer exceeds the collector inlet temperature by at least 30°F.

Mode 4 - Collector-to-Water Preheating: This summer operation mode is entered when two conditions are met. The first condition is that there is a request for hot water. The second condition occurs when the collector outlet temperature exceeds the gymnasium temperature by 45°F. Heated air drawn from the collector is circulated via the air-handling unit through the ducts past an air-to-liquid heat exchanger and returned

to the collector (the air bypasses the rock thermal storage). Simultaneous to collector air flow, pump Pl is turned on and DHW preheat tank water is circulated through the air-to-liquid heat exchanger, where solar energy is obtained and used to increase the temperature of the DHW preheat tank. This mode continues until the temperature in the preheat tanks reaches 140°F, or until the collector outlet temperature no longer exceeds the collector inlet temperature by at least 30°F. This preheated water is stored in two 120-gallon tanks and delivered on demand to the 52-gallon DHW heater. Water can also be preheated in Modes 1 and 3 during the heating season, when energy collection is occurring and a hot water demand exists.

Mode 5 - Grain Drying: This manually controlled winter mode is utilized to reduce the moisture of grain stored in a bin near the gymnasium. This mode operates in the fall and spring to utilize excess solar energy.

Manual dampers D8 and D5 (Figure 1) are opened, and manual dampers D4, D6 and D7 are closed. This action provides a path for outside air to be drawn by the air-handling unit through the collectors, where it is heated, and then supplied to the grain bin. The mode is entered by raising the gymnasium thermostat to artificially produce a demand for space heating to the control system. The mode is terminated manually either after solar energy is exhausted, or after the grain reaches the desired dryness.

II. PERFORMANCE EVALUATION

The system performance evaluations discussed in this section are based primarily on the analysis of the data presented in the attached computer-generated monthly report. This attached report consists of daily site thermal and energy values for each subsystem, plus environmental data. The performance factors discussed in this report are based upon the definitions contained in NBSIR 76-1137, Thermal Data Requirements and Performance Evaluations Procedures for the National Solar Heating and Cooling Demonstration Program.

A. Introduction

The Scattergood School solar energy system operated in the winter space heating modes until June 25, 1979, when the system was converted to summer operation. The system furnished 97 percent of the 12.13 million Btu required to satisfy the combined space heating and hot water demand. The operation of these subsystems resulted in a savings of 19.19 million Btu of fossil fuel energy (210 gallons of propane) at an expense of 0.28 million Btu of electrical energy (83 kwh).

B. Weather

The insolation available on the collector array during the month was an average of 1,500 Btu/ft 2 -day, which is near the 1,579 Btu/ft 2 -day estimated for the month. This estimate is computed by using an algorithm to estimate the insolation on a tilted surface from long-term insolation data (on a horizontal surface) obtained from <u>SOLMET Volume 1 - User's Manual</u>. The horizontal insolation data from Des Moines, Iowa and Moline, Illinois were used to estimate the horizontal insolation for Westbranch, Iowa.

The average measured outside ambient temperature was 70°F, which is 1°F lower than the 71°F long-term prediction from the average of Des Moines, Iowa and Moline, Illinois temperature data obtained from <u>Climatography of the United States No. 81</u> (By State).

C. System Thermal Performance

<u>Collector</u> - Of the 112.33 million Btu of incident solar energy on the collector array during June, 60.24 million Btu were incident on the array when the collector was operating. The system collected 18.47 million Btu, or 16 percent of the available insolation at an expense of 0.28 million Btu of electrical operating energy. The system collected 30 percent of the insolation available during collector operation.

From collected energy, 3.19 million Btu were delivered to the hot water preheat tanks, 8.69 million Btu were delivered to storage, and 6.45 million Btu were delivered directly to the loads. Consequently, there was an indicated loss of approximately 3.33 million Btu from the transport loops in the subsystem.

Storage - The rock thermal storage subsystem received 8.69 million Btu of collected solar energy. The subsystem furnished 5.07 million Btu to meet the space heating demand. The energy lost from storage amounted to 1.84 million Btu. A portion of the storage energy loss is believed to have been transmitted to the gymnasium, thus contributing to the cooling requirements of the gymnasium. The monthly storage efficiency was 56 percent. The storage subsystem was bypassed, beginning July 25, when the system was converted to the summer mode.

Domestic Hot Water Load - Hot water consumption for the month was 1,076 gallons, or 36 gallons per day. The hot water load was 0.62 million Btu, of which 50 percent was supplied by solar energy. In order to satisfy this load and to maintain the DHW supply at an average temperature of 134°F, 4.04 million Btu of thermal energy were supplied to the DHW and preheat tanks. The difference between the energy added to the tanks and the hot water load are thermal losses from the DHW subsystem. The total thermal loss from the subsystem was 3.42 million Btu. The 4.04 million Btu of energy transferred to the DHW heater and two preheat tanks were comprised of 3.19 million Btu of solar energy, and 0.85 million Btu of auxiliary thermal energy supplied to the DHW heater. (A septic tank problem at the boy's dormitory in the past month necessitated increased use of the DHW subsystem in the recreation center. This increased usage resulted in a performance increase of the subsystem during the month.)

<u>Space Heating Load</u> - To maintain an average indoor temperature of 79°F for the gymnasium, the solar energy system at Scattergood School provided 100 percent of the indicated space heating demand of 11.52 million Btu.

The space heating demand for June was expected to be 0.48 million Btu. However, the actual space heating demand was 11.52 million Btu. The discrepancy between the expected and actual space heating demands is due to excess solar energy contributions to the gymnasium. A motorized damper leak and natural convection transfer of energy from rock storage are the sources of the excess solar heating. This condition is discussed in detail in the observation section of this report.

D. Observations

The large transport loop energy losses may be caused by leakage through manual slide dampers. The leaky dampers could result from inadequate sealing of the manual dampers after the solar energy system was converted from the summer to winter operation in October 1978, and from grain drying operation to space heating in November 1978. Another source of transport loop leakage is the collector plenums. As the system ages, the connections between the collectors and the plenums may begin to leak. An investigation will be performed to ascertain the cause of the collector transport leaks during checkout of the additional measurement sensors to be installed next month.

The excess solar energy delivered to the gymnasium was caused by two situations. First, the solar system was operated generally in the storage and hot water preheating modes due to the lack of a space heating load during the month. In the hot water or rock storage heating modes, a 12 percent leak rate in motorized damper MD-2 allowed energy to be transferred to the gymnasium. During these periods, the gymnasium temperature rises to approximately 80°F. An average gymnasium temperature of 79°F illustrates the effect of the leak. This condition resulted in the transfer of 6.45 million Btu to the gymnasium, which alone was more than sufficient to satisfy the heating demand for this month.

A second source of solar energy results from a continuous low-level natural convection transfer of energy from the rock thermal storage to the gymnasium. The natural convection flow results from a chimney effect produced by the combined effects of a tall gymnasium, cold gymnasium temperatures, and a hot storage which by design is open to the gymnasium when the solar energy system is de-energized. This condition resulted in the transfer of approximately 5.07 million Btu to the gymnasium.

To create habitable conditions in the gymnasium, a propeller exhaust fan in combination with an open gymnasium access door was utilized to remove excess energy in the gymnasium. Thus, additional energy was utilized to run the propeller fan during the summer because of the excess solar energy added to the site.

The leaky motorized damper MD-2 should be adjusted to eliminate the air leak to the gymnasium and the rock thermal storage bypassed to prevent the excess thermal energy transfer to the building during the summer months.

E. Energy Savings

Solar energy space heating savings were 19.19 million Btu of fossil energy (210 gallons of propane) that was obtained at an expense of 0.28 million Btu of electrical energy. The low space heating operating expense is the result of two factors. First, a continuous low-level natural convection transfer of energy exists from the rock thermal storage to the gymnasium. Second, during the day when the solar energy system is heating hot water, a 12 percent leak rate in motorized damper MD-2 (Figure 1) is allowing solar energy to be transferred to the building. This reduces the requirement for controlled transfer using the circulation fan, thus reducing the operating expense.

Energy savings calculations are based on a comparison of the energy requirements of a conventional propane-fired furnace, with an assumed burning efficiency of 60 percent, to the requirements of the solar energy system.

The hot water subsystem operation resulted in an electrical energy savings of 0.31 million Btu (91 kwh). The energy savings calculations are based on a comparison of the projected energy requirements of a conventional electrical hot water tank to the energy requirement of the solar energy system. All energy requirements are based on the measured demand for hot water.

III. ACTION STATUS

Instrumentation designed to measure more accurately the hot water subsystem performance and to measure storage subsystem air flow has been specified. These additional sensors, along with the Materials Assessment Program package, have been sent to the site. The additional sensors were installed during the last week of June. Sensor checkout and data system refurbishment will occur in mid-July.

Grain drying air flow sensor W410 is inoperative. The sensor will be repaired in conjunction with the checkout. Storage return temperature sensor T151 and hot water heat exchange temperature T304 have malfunctioned numerous times since November 1978. During these periods, measurement T202 was substituted for measurement T151 and T352 substituted for T304. Sensors T151 and T304 will also be repaired during checkout.

PRC FATICA CNST 2. 0 Ů CCCLIA AND ATING

EPORT 0 ≥ > U ĪΨ CNT

≥

SCL AR/2003-	
SCHCCL E,1979	
ATTERGOOD SUN	
RE CRY PE	

0/6

SCATTERGOOD IS A HIGH SCHCCL WITH AN ENRCLLMENT OF SCATTERGOOD IS A HIGH SCHCCL WITH AN ENRCLLMENT OF SIXTY STUDENTS. THE SCLAR SYSTEM PROVIDES HEAT AND HOT WATER FOR A 7.966 SQ.FT. GYMNASIUM. THE SYSTEM UTILIZES AIR AS THE CIRCULATING HEAT TRANSFER MEDIUM AND A 62 TON PEBELE BED FOR STORAGE. AUXILIARY HEATING I PROVIDED BY TWO 250K ETU AND CNE 100K BTU PROPANE HEATERS. HOT WATER AUXILLIARY IS A 4.5KW ELECTRIC ELEMENT IN THE DOMESTIC HOT WATER TANK. U

MILLION BTU BTU/SO.FT. FILLION BTU BTU/SO.FT. DEGREES F LLL ION 18.5.334 18.5.006 18.5.006 18.5.006 18.5.006 19.5.0 greet greet AVERAGE AMBIENT TEMPERATURE
AVERAGE BUTLDING TEMPERATURE
ECSS SCLAR CCNVERSION EFFICIEN
ECSS CPERATING ENERGY
TOTAL SYSTEW CPERATING ENERGY
TOTAL ENERGY CONSUMED FGY BNER Ш Z W SCLAR <(SOL SITE ECTE! RAL COLL Ш ⋈ Z

BTC BTC

 \Box 1 17000 *5* 0 0 SCLAR FRACTION
SCLAR ENERGY USED
CPERATING ENERGY
AUX. THERMAL ENERGY
AUX. FCSSIL FUEL
AUX. FCSSIL FUEL
FCSSIL SAVINGS ARY Z Z Ш F 57 > 51 8000

. Ø CTCR CA ш UNAVAILABLE NULL DATA ES NOT APPLI ٩ ш EFFCFMANCE DENCHES DENCHES DENCHES Ü 15 # BZ

, 197 PERFORMANCE REPORT FCGRAN, FEERUARY 28 ᄔ > GUIDE TO THE MONTHLY NATIONAL SCLAF DATA 004-78/18 AR/O 0 SEL 200 ш FERENC

ш

CABL

Н

Ш

SCLAR FEATING AND COCLING DEMONSTRATION PROGRAM

TEL SCATTERCCCD SCHCCL PERIOD: JUNE, 1575 TEL/SYSTEM DESCRIPTION: SCHCCL SCATTERCCCD SCHCCL SCATTERCCCD SCHCCL SCATTERCCCD SCHCCL SCATTERCCCD SCHCCL SCATTERCCCD SCHCCL TASSER MEDIUM AND A 62 TCM FEELE EED FOR STICRAGE AUXILIARY HEATTNG TS.966 SG.FT THE CLAFE SYSTEM FECTATIOS ENGRETISE AUXILIARY HEATTNG TS.966 SG.FT THE CLAFE SYSTEM FECTATIOS ENGRETISE AUXILIARY HEATTNG TS.966 SG.FT TASSER MEDIUM AND A 62 TCM FEELE EED FOR STICRAGE AUXILIARY HEATTNG TS.966 SG.FT TASSER MEDIUM AND A 62 TCM FEELE EED FOR STICRAGE AUXILIARY HEATTNG TS.966 SG.FT TANK TELEDATA: TS.967 SCHCAR STICRAGE AUXILIARY HEATTNG TS.967 SCHCAR TANK TO COLLECTED SCLAR ENERGY TO COLLECTED SCLAR	FOSSIL SAVINGS N.A. 20.248 N.A. 20.248 GIGA JOULE TEM FEFFCFMANCE FACTOR: Denotes unavailable data	CLAR FRACTION		VERAGE AMBIENT TEMPERATURE VERAGE EUILDING TEMPERATURE CSS SOLAR CONVERSION EFFICIENCY CSS CPERATING ENERGY O.873 GIGA JOULE	CLLECTED SCLAR ENERGY 19.485 GIGA JOULE	ERAL SITE DATA: INCIDENT SCLAR ENERGY	SCATTERGEED IS A HIGH SCHOOL WITH AN ENROLLMENT OF SIXTY STUDENTS. THE SCHOOL WITH AN ENROLLMENT OF 7,966 SG.FT. GYMNASIUM. THE SYSTEM UTILIZES AIR AS THE CIRCULATING HEAT TRANSFER REDIUM AND A 62 TCN PEEBLE BED FOR STORAGE. AUXILIARY HEATING IS PROVIDED BY TWO 250K BIL AND ONE 100K BTL PROPANE HEATERS. HOT WATER AUXILLIARY IS A 4.55KW ELECTRIC ELEMENT IN THE DOMESTIC FOT WATER TANK.	E: SCATTERGOOD SCHOOL CRT PERIOD: JUNE-1979	CATHLY REPOR
---	--	---------------	--	--	---	--	--	---	--------------

USER'S GUIDE TO THE MONTHLY PERFORMANCE REPORT OF THE NATIONAL SCLAF DATA FFOGRAM.FEERUARY 28,1978, SCLAR/0004-78/18

REFERENCE:

SCLAR PEATING AND COCLING DEMCNSTRATION PROGRAM

ENERGY CCLLECTION AND STORAGE SUBSYSTEM (ECSS)

	ECSS SOLAR CONVERSION D EFFICIENCY	00000000000000000000000000000000000000	1 1	0.131
	ECSS ENERGY REJECTEI MILLICE	MCB>ACZ	Z • A • I	•
	SHEHD	00000000000000000000000000000000000000	0.568	• 1
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	AUX THERMAL TC ECSS MILLION BTU	MCMACUMA 407	A	0 1
1 1 1 1	NERG TC CADS LLLIC ETU	00000000000000000000000000000000000000	14.705	C • 490
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	AVELENT TEMP OEG-F	2011 2011 2011 2011 2011 2011 2011 2011		70
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	INCIDENT SCLAR ENERGY FILLICA BTU	4041)440 400444 4440 4040 4	112,334	3.744
	M CO A Y		SUM	AVG

* DENOTES UNAVAILABLE CATA. a DENOTES NULL DATA. N.A. DENOTES NOT APPLICABLE CATA.

SOLAR PEATING AND CCCLING DEMCNSTRATION FROGRAM

COLLECTOR ARRAY PERFORMANCE

SITE: SCATTERGOCD SCHCCL REPORT PERICD: JUNE, 1979

SOLAR/2003-79/06

COLLECTOR ARRAY EFFICIENCY	00000000000000000000000000000000000000			2100
CAYTIME AMBIENT TEMP DEG F	7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	† 	76	1 1 1 1 1 1 1
CCLLECTED SOLAR ENERGY MILLICN ETU		18.465	0.616	0100
CFERATICNAL INCIDENT ENEFGY WICLICN	WUNHUUOOUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUU	60.236	2.008	
INCIDENT SOLAR ENEFGY MILLION	4m4m44m=m4mm44mm4444=444mm44 40mm4 40mm4mmmmmmmmmmmmmmmmm	112.334	-	0001
M CO A Y H		SUM	>	NBSID

* DENOTES UNAVAILABLE CATA.

© DENOTES NULL CATA.

N.A. DENOTES NCT APPLICABLE DATA.

SOLAR PEATING AND CCCLING DEMCNSTRATION PROGRAM

STURAGE PERFORMANCE

0			
R/2003-79/0	STORAGE		N100
SOLA	STORAGE AVERAGE TEMP DEG F	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
•	CHANGE IN STORED ENERGY FILLION BTC		G202
ATTERGOOD SCHCCL ERICC: JUNE,1979	ENERGY FRCM STCRAGE WILLICN BTU	00000000000000000000000000000000000000	G201
		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	G 2 0 0
SITE: SCA REFCRT PE	M C C C C C C C C C C C C C C C C C C C		LES ID

* DENCTES UNAVAILAELE CATA. a denotes null data. N.A. Denctes nct Applicaele data.

SBLAR/2003-75/06

ر	0
Ö	11979
I	\rightarrow
Ü	-
SCHOOL	
	JUNE
	\supset
0	7
9	0.0
α	
ERGOOD	\cup
SCATT	ICC
\vdash	E
⋖	ш
U	O.
S	
	-
0.0	α
SITE:	
\vdash	0
	ш
S	C

1 00	M	
WATE USE GAL		0
HE H		n i
SUNDI MANDI DEGNO	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	o i
FCSSIL FCSSIL ENERGY SAVINGS MILLION ETU		5
ELECT ELECT ENERGY SAVINGS MILLION BTU	00000000000000000000000000000000000000	7
AUX FCSSIL FUEL WILLION	A I A I A I A I A I A I A I A I A I A I	o i
A TELECT FLECT FLECT FIELICN	00000000000000000000000000000000000000	
T PERWAL NICSED NICLICA	00000000000000000000000000000000000000	o i
1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		0
AAMHU		
	į į į į į į į į į į į į į į į į į į į	o i
	000000000000000000000000000000000000	0
M D A Y		

* DENCTES UNAVAILABLE DATA. @ DENCTES NULL CATA. N.A. DENOTES NCT APPLICABLE CATA. SOLAR PEATING AND COCLING DEMONSTRATION PROGRAM

SFACE PEATING SUBSYSTEM

SITE: SCATTERGOCD SCHOOL REPORT PERICO: JUNE, 1979

SOLAR/2003-79/06

AKB DEG D	0	700	N113
BLDG TEMP DEG.		79	N406
FCSSIL FCSSIL ENERGY MILLION PTUON	00000000000000000000000000000000000000	19.193	G417
M ILLINGS MILLINGS		-0.026	6415
		0000	6410
ELECT FLECT FLECT NICLICN	MCMACDDA 407	• • • • • • • • • •	
AUX THERMAL USED NILLICA		000000	G4C1
7 4	U0U000U0U0U00U0U0000000000000000000000	0101	0402
1 > 4		• 51 • 52 • 52 • 52 • 52 • 53 • 54	0400
SCLAR FR.CF LCAO PCT		100	
		NIWI	0402
10 X 100 X 17 Y Y		SUX A V G	

* DENCTES UNAVAILABLE DATA. D DENCTES NULL CATA. N.A. DENOTES NCT APPLICABLE CATA.

SCLAR HEATING AND CCCLING DEMONSTRATION PROGRAM

MCNTHLY REPORT ENVIRONMENTAL SUMMARY

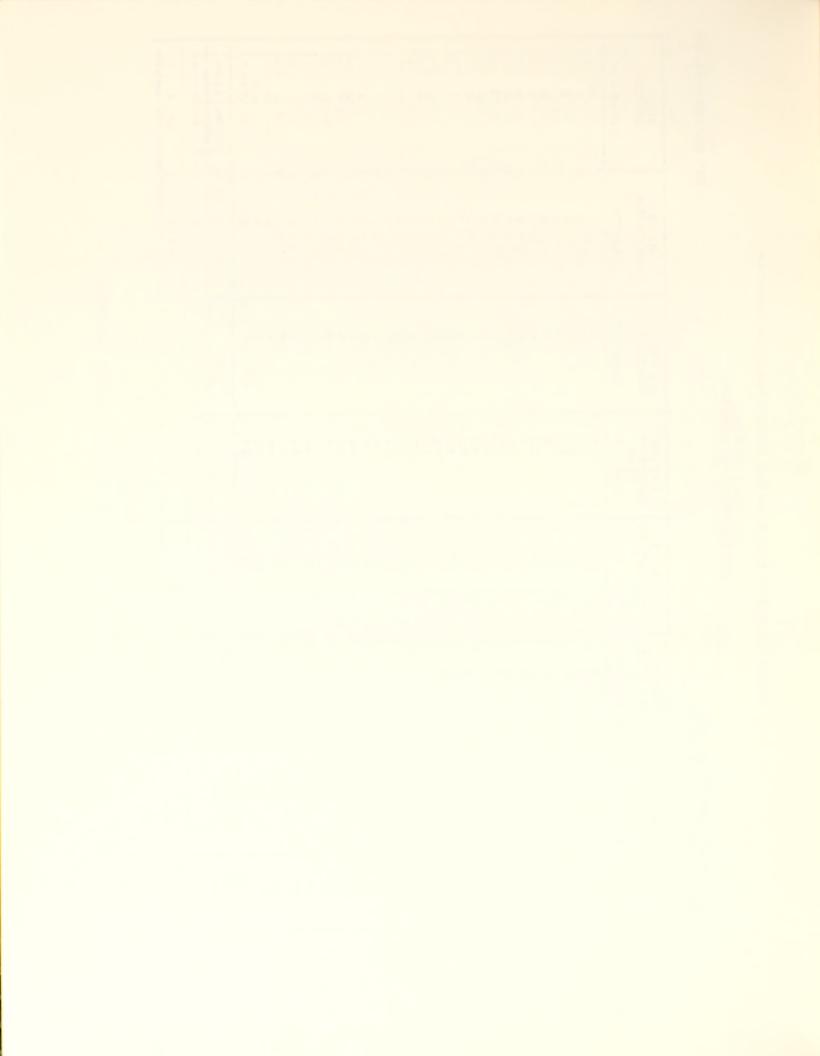
SCATTERGOOD SCHOOL

SITE:

SCL AR/2003-79/06

		l l		1
S DEED SPEED W. D. H.	000m00000m000000m000000m0000		with winn man with rate of the same winn that the same winn that the same winner that the sam	サーニス
WIND DIRECTION DEGREES	()			S Z
RELATIVE HUMIDITY PERCENT	*************		.4.6	the state of the calls
DAYTIME AMEIENT TEMP DEG F	01111111111111111111111111111111111111		1(1)	e vein d'ès cele ann que que de la comme que
TEMPERATURE CEG F	0		20	
CIFFUS NSCLATI ETU/SQ.	COF GCT™ CAMTM	0 0	9 9	
TIOI FT			(ی	0
MCNTH	*************************************	ا ر	A V G	00 Z

* DENCIES UNAVAILAELE CATA. â dengies null data. N.A. dencies nci applicaele cata.







UNIVERSITY OF FLORIDA 3 1262 09052 6707